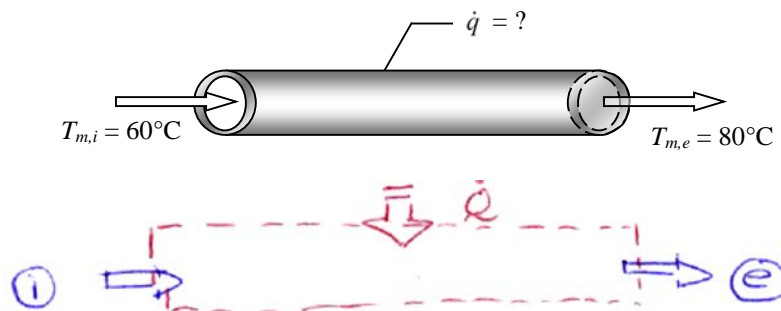


## Example

Water flows through a section of 2.54-cm diameter tube 3.0 m long. The water enters the section at 60°C with a velocity of 2 cm/s. Assuming that the flow is **fully developed** (buzza buzza buzza) by the time it enters the region of interest and that the wall is subject to constant wall heat flux,

- calculate the wall heat flux (in W/m<sup>2</sup>) needed to heat the water to 80°C.
- Calculate the wall temperatures at the inlet and the exit.
- Repeat part a) and b) if the velocity of the water is increased to 2 m/s.



### Fluid properties

$$T_B = \frac{T_i + T_e}{2} = 70^\circ\text{C}$$

$$\rho = 977.5 \text{ kg/m}^3$$

$$\mu = 0.404 \times 10^{-3} \text{ kg/m}\cdot\text{s}$$

$$k = 0.663 \text{ W/m}\cdot\text{K}$$

$$c_p = 4190 \text{ J/kg}\cdot^\circ\text{C}$$

$$Pr = 2.55$$

(a) Use cons. of energy:

$$0 = \dot{Q} + 0 + \dot{m} h_i - \dot{m} h_e$$

$$\dot{Q} = \dot{m}(h_e - h_i) = \dot{m} [c_p(T_e - T_i) + v(\cancel{P_e - P_i})]$$

$$= (9.906 \times 10^{-3} \frac{\text{kg}}{\text{s}}) (4190 \frac{\text{J}}{\text{kg}\cdot^\circ\text{C}}) (80^\circ\text{C} - 60^\circ\text{C})$$

$$= 830 \text{ W}$$

$$\dot{q} = \frac{\dot{Q}}{A_{\text{SURFACE}}} = \frac{\dot{Q}}{\pi D L} = \frac{860 \text{ W}}{(\pi)(0.0254 \text{ m})(3.0 \text{ m})} = \boxed{3468 \text{ W/m}^2}$$



NOT  $A_{\text{CROSS-SECTION}}$  !

$$\begin{aligned} \dot{m} &= \rho A V = \rho \frac{\pi D^2}{4} \cdot v \\ &= 977.5 \frac{\text{kg}}{\text{m}^3} \cdot \frac{\pi \cdot 0.0254^2 \text{ m}^2}{4} \cdot 0.02 \frac{\text{m}}{\text{s}} \\ &= \underline{\underline{9.906 \times 10^{-3} \text{ kg/s}}} \end{aligned}$$

(b) Since we want wall temperatures, we need:

$$\dot{q}_b = h(T_{s,e} - T_e) \quad \& \quad \dot{q}_b = h(T_{s,i} - T_i)$$

If we can find  $h$ , we've got it.

$$Re = \frac{\rho V D}{\mu} = \frac{977.5 \frac{\text{kg}}{\text{m}^3} \cdot 0.02 \frac{\text{m}}{\text{s}} \cdot 0.0254 \text{ m}}{0.464 \times 10^{-3} \frac{\text{kg}}{\text{m} \cdot \text{s}}} = 1229$$

↳ LAMINAR FLOW

- Laminar
  - Fully-developed
  - Round duct
  - $\dot{q} = \text{const}$  BC
- ...  $Nu = 4.36$

$$Nu = \frac{hD}{k} \rightarrow h = \frac{Nu \cdot k}{D} = \frac{(4.36)(0.663 \frac{\text{W}}{\text{m} \cdot \text{C}})}{0.0254 \text{ m}} = 113.9 \frac{\text{W}}{\text{m}^2 \cdot \text{C}}$$

At inlet:

$$\dot{q}_b = h(T_{s,i} - T_i) \quad T_{s,i} = T_i + \frac{\dot{q}_b}{h} = 60^\circ\text{C} + \frac{3468 \text{ W/m}^2}{113.9 \text{ W/m}^2 \cdot \text{C}}$$

$T_{s,i} = 90.4^\circ\text{C}$

At exit:

$$\dot{q}_b = h(T_{s,e} - T_e) \quad T_{s,e} = T_e + \frac{\dot{q}_b}{h} = 80^\circ\text{C} + \frac{3468 \text{ W/m}^2}{113.9 \text{ W/m}^2 \cdot \text{C}}$$

$T_{s,e} = 100.4^\circ\text{C}$

Remember, w/  $\dot{q} = \text{const}$  BC & fully-developed flow,  $T_s - T_m$  is the same @ all locations.

(c) The process is the same, the numbers change. Here are the highlights:

$$\dot{m} = \dots = 0.9906 \text{ kg/s}$$

$$\dot{Q} = \dots = 83,000 \text{ W}$$

$$\dot{q} = \dots = 343,715 \text{ W/m}^2$$

$$Re = \dots = 122,900 \longrightarrow \text{TURBULENT FLOW}$$

- Turbulent
  - Fully-developed
  - Round duct
  - $\dot{q} = \text{const B.C.}$
- Many choices.

One easy one:

$$\begin{aligned} Nu &= 0.023 Re^{0.8} Pr^{0.4} \\ &= (0.023)(122,900)^{0.8} (2.55)^{0.4} \\ &= 394 \end{aligned}$$

$$h = \frac{Nu \cdot k}{D} = \frac{(394)(0.663 \text{ W/m}\cdot\text{K})}{0.0254 \text{ m}} = \underline{10,295 \text{ W/m}^2\cdot\text{C}}$$

Note how much higher!

$$\text{Inlet: } T_{s,i} = T_i + \frac{\dot{q}}{h} = \dots = 93.7^\circ\text{C}$$

$$T_{s,e} = T_{s,e} + \frac{\dot{q}}{h} = \dots = 113.7^\circ\text{C}$$

For turbulent flow, a  $T_s - T_m$  of a little over  $10^\circ\text{C}$  gives  $100\times$  more  $\dot{q}$  than for laminar flow.