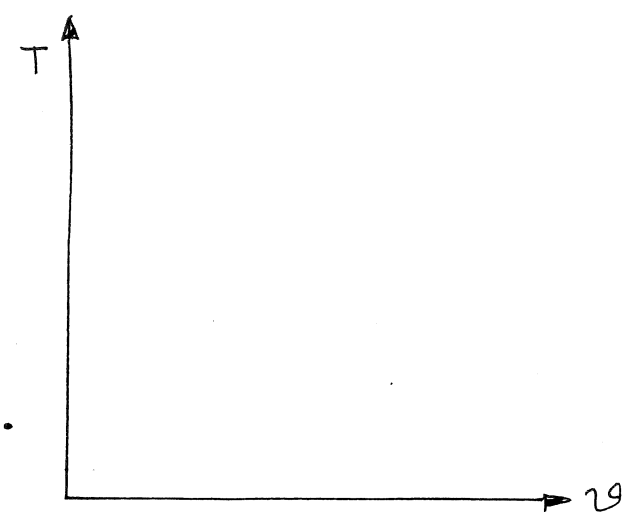




DRAW A GENERIC T-U DIAGRAM.*



◦ NOW REPLACE _____ WITH _____.

◦ ALL THE TRENDS ARE THE SAME ◻

◦ But why do we care? ~~∞~~

ENTROPY ACCOUNTING →

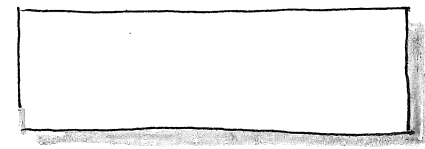
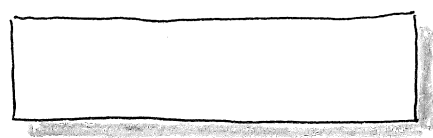
$$\frac{d}{dt}(S_{SYS}) = \sum \frac{\dot{Q}_{in}}{T_b} + \sum \dot{m}_i \Delta - \sum \dot{m}_{out} \Delta + \dot{S}_{gen}$$

CLOSED SYS, FINITE TIME
+ INTERNALLY REVERSIBLE

OPEN, S-S SYS, 1 INLET & 1 EXIT
+ INTERNALLY REVERSIBLE

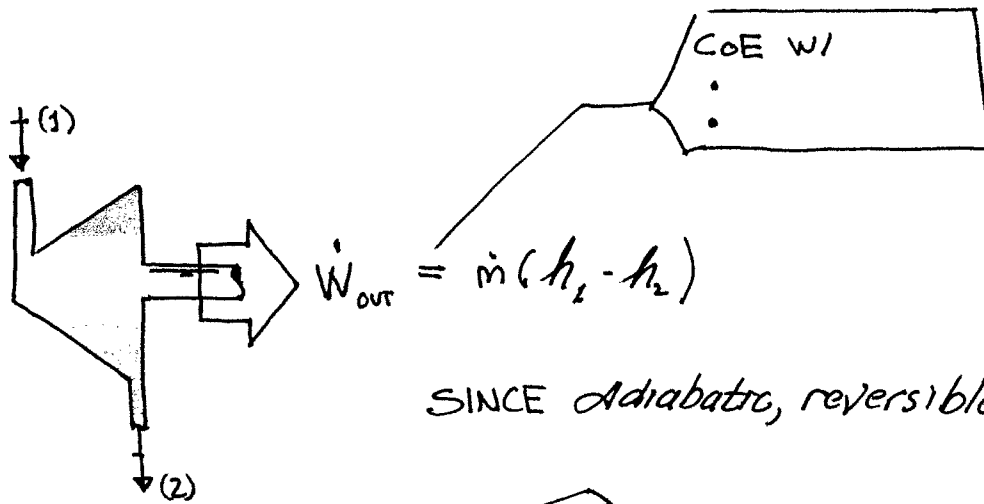
PICK SYSTEM SO THAT $T_b = T_{SYS}$

PICK SYSTEM SO THAT $T_b = T_{SYS}$

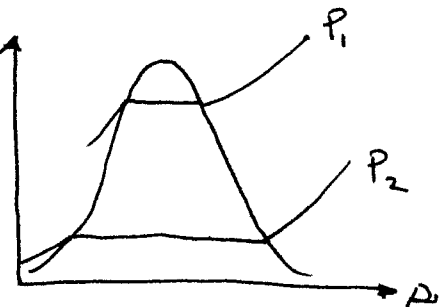
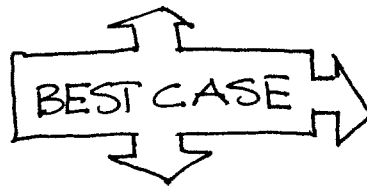


* BE SURE TO LABEL THE PHASES & SHOW LINES of CONST. P.

LET'S RE-EXAMINE THE TURBINE
IN THE LAST EXAMPLE.



SINCE *adiabatic, reversible* \Rightarrow _____



WRITE S-ACCT'ING FOR A REAL (i.e., ADIABATIC BUT IRREVERSIBLE) TURBINE

$$\frac{dS_{sys}}{dt} = \sum \frac{\dot{Q}}{T_b} + \sum_{in} \dot{m} \Delta s - \sum_{out} \dot{m} \Delta s + \dot{S}_{GEN}$$

$$\Delta s_{2, ACTUAL}$$

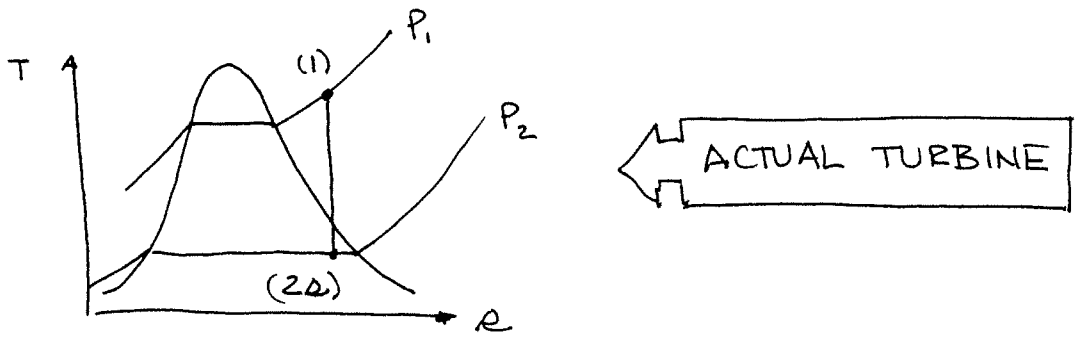
$$>, <, = \Delta s_{2, IDEAL}$$

$$\therefore h_{2, ACTUAL} = h(P_2, \Delta s_{2, ACTUAL}, \Delta s_{2, IDEAL})$$

$$>, <, = h_{2, IDEAL}$$

$$\therefore \dot{W}_{out, ACT} = \dot{m}(h_1 - h_{2, ACTUAL})$$

$$>, <, = \dot{W}_{out, IDEAL}$$



(2D) SIGNIFIES _____ (IDEAL) TURBINE

(2) " _____ "

----- WHY THE DASHED LINE FOR THE ACTUAL TURBINE?

ANS:



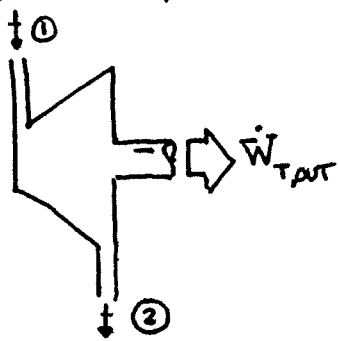
LET US DEFINE, THEN

$\eta_T \equiv$ _____

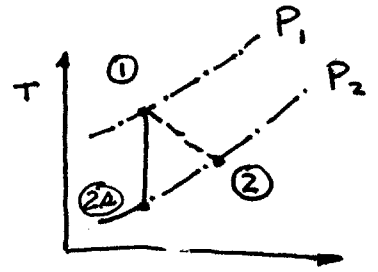
↑

ISENTROPIC (A.K.A ADIABATIC) EFFICIENCIES

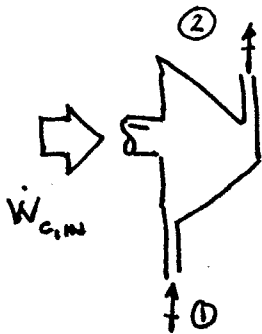
TURBINE



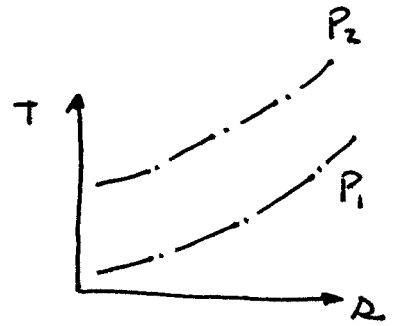
$$\eta_T \equiv \frac{\dot{W}_{out}}{\dot{W}_{out,s}} = \frac{\dot{m}(h_1 - h_2)}{\dot{m}(h_1 - h_{2s})}$$



COMPRESSOR



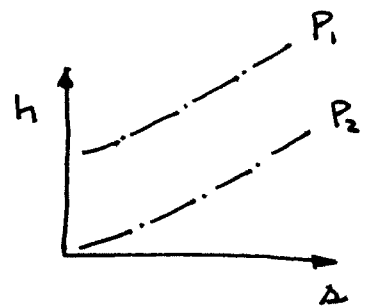
$$\eta_c \equiv \frac{\dot{W}}{\dot{W}} = \text{_____}$$



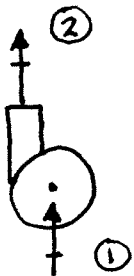
NOZZLE



$$\eta_N \equiv \frac{\Delta KE}{\Delta KE_s} = \text{_____}$$



PUMP



$$\eta_P \equiv \text{_____}$$