

Name Solutions

ECE 320
Linear Control Systems

Exam 2
Winter 2015-2016

- This exam is closed-book in nature.
- No calculators or computers (except for music)
- Clearly indicate your answer and include units, labels, etc. as appropriate

Problem 1 _____/18
Problem 2 _____/20
Problem 3 _____/13
Problem 4 _____/16
Problems 5-15 _____/33

Exam ~~3~~₂ Score: _____ / 100

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- 1) For each of the following transfer functions determined from state variable models using state variable feedback, with two states, determine if the system is controllable or not

$$G_o(s) = \frac{1}{s^2 + k_2 s + 1} \quad \checkmark$$

$$G_o(s) = \frac{1}{(s - k_1)(s - k_2)} \quad \checkmark$$

$$G_o(s) = \frac{1}{(s - k_1 k_2)^2} \quad \checkmark$$

$$G_o(s) = \frac{1}{s + k_2} \quad \checkmark$$

$$G_o(s) = \frac{1}{s^2 + k_1 k_2 s + (3 - k_1)} \quad \checkmark$$

$$G_o(s) = \frac{(s + k_1)}{(s + k_1)(s + k_2 + 1)} \quad \checkmark$$

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2) For the following state variable system

$$\dot{x}(t) = \begin{bmatrix} 1 & 2 \\ 3 & 0 \end{bmatrix} x(t) + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u(t)$$

$$y(t) = [1 \ 0] x(t)$$

with state variable feedback $u(t) = G_{pf}r(t) - Kx(t)$, determine the closed loop transfer function between the input $R(s)$ and the output $Y(s)$.

$$\tilde{A} = A - BK = \begin{bmatrix} 1 & 2 \\ 3 & 0 \end{bmatrix} - \begin{bmatrix} 0 & 0 \\ k_1 & k_2 \end{bmatrix} = \begin{bmatrix} 1 & 2 \\ 3 - k_1 & -k_2 \end{bmatrix}$$

$$sI - \tilde{A} = \begin{bmatrix} s & 0 \\ 0 & s \end{bmatrix} - \begin{bmatrix} 1 & 2 \\ 3 - k_1 & -k_2 \end{bmatrix} = \begin{bmatrix} s-1 & -2 \\ k_1-3 & s+k_2 \end{bmatrix}$$

$$(sI - \tilde{A})^{-1} = \frac{1}{(s-1)(s+k_2) + 2(k_1-3)} \begin{bmatrix} s+k_2 & 2 \\ 3-k_1 & s-1 \end{bmatrix} = \frac{1}{\Delta(s)} \begin{bmatrix} s+k_2 & 2 \\ 3-k_1 & s-1 \end{bmatrix}$$

$$G_0(s) = C(sI - \tilde{A})^{-1} \tilde{B} = \frac{[1 \ 0]}{\Delta(s)} \begin{bmatrix} s+k_2 & 2 \\ 3-k_1 & s-1 \end{bmatrix} \begin{bmatrix} 0 \\ G_{pf} \end{bmatrix} = \frac{2 G_{pf}}{(s-1)(s+k_2) + 2(k_1-3)} = G_0(s)$$

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3) Consider the following transfer function $G_o(s) = \frac{\alpha}{s^2 + 2\alpha s + \omega_o^2}$

- a) Determine the sensitivity of this transfer function to variations in α . For full credit your answer must be the ratio of two polynomials.
 b) Determine an expression for the sensitivity as a function of frequency.

$$\int_{\alpha}^{G_o} = \frac{\alpha}{N} \frac{\partial N}{\partial \alpha} - \frac{\alpha}{D} \frac{\partial D}{\partial \alpha}$$

$$= \frac{\alpha}{\alpha} (1) - \frac{\alpha}{s^2 + 2\alpha s + \omega_o^2} (2s) = 1 - \frac{2\alpha s}{s^2 + 2\alpha s + \omega_o^2}$$

$$= \frac{s^2 + \omega_o^2}{s^2 + 2\alpha s + \omega_o^2} = \int_{\alpha}^{G_o}$$

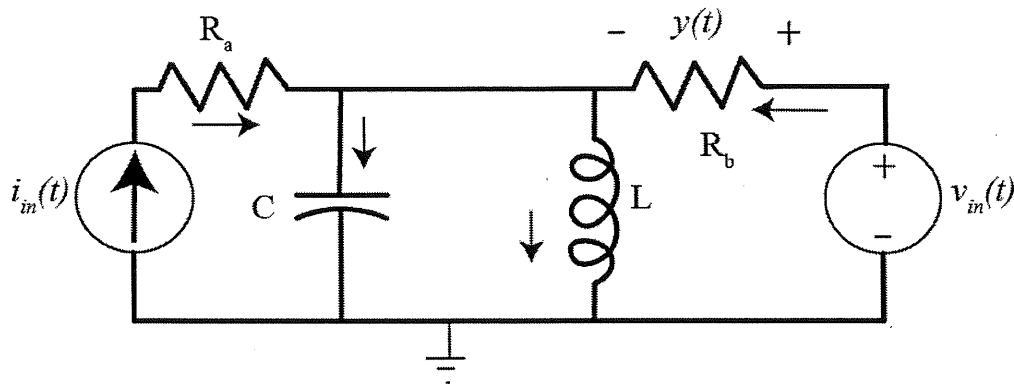
$$\int_{\alpha}^{G_o}(j\omega) = \frac{-\omega^2 + \omega_o^2}{-\omega^2 + 2\alpha j\omega + \omega_o^2}$$

$$\left| \int_{\alpha}^{G_o}(j\omega) \right| = \frac{\sqrt{(\omega_o^2 - \omega^2)^2}}{\sqrt{(\omega_o^2 - \omega^2)^2 + 4\alpha^2 \omega^2}}$$

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- 4) For the following circuit, determine a state variable representation. Assume the currents flow in the directions shown, the output is $y(t)$, the first state is $v_C(t)$ and the second state is $i_L(t)$.

Recall that $i_C(t) = C \frac{dv_C(t)}{dt}$ $v_L(t) = L \frac{di_L(t)}{dt}$



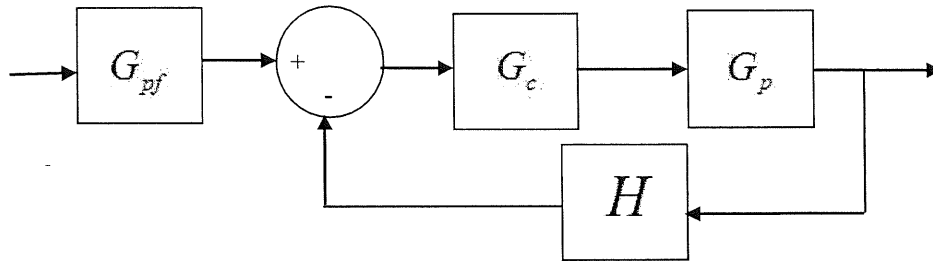
$$i_{in}(t) + \frac{v_{in}(t) - v_C(t)}{R_b} = C \frac{dv_C(t)}{dt} + i_L(t) \quad L \frac{di_L(t)}{dt} = v_C(t) \quad y(t) = v_{in}(t) - v_C(t)$$

$$\frac{dv_C(t)}{dt} = -\frac{1}{R_b C} v_C(t) - \frac{1}{C} i_L(t) + \frac{1}{C} i_{in}(t) + \frac{1}{R_b C} v_{in}(t) \quad \frac{di_L(t)}{dt} = \frac{1}{L} v_C(t)$$

$$\frac{d}{dt} \begin{bmatrix} v_C(t) \\ i_L(t) \end{bmatrix} = \underbrace{\begin{bmatrix} -\frac{1}{R_b C} & -\frac{1}{C} \\ \frac{1}{L} & 0 \end{bmatrix}}_A \begin{bmatrix} v_C(t) \\ i_L(t) \end{bmatrix} + \underbrace{\begin{bmatrix} \frac{1}{R_b C} & \frac{1}{C} \\ 0 & 0 \end{bmatrix}}_B \begin{bmatrix} v_{in}(t) \\ i_{in}(t) \end{bmatrix}$$

$$y(t) = \underbrace{\begin{bmatrix} -1 & 0 \end{bmatrix}}_C \begin{bmatrix} v_C(t) \\ i_L(t) \end{bmatrix} + \underbrace{\begin{bmatrix} 1 & 0 \end{bmatrix}}_D \begin{bmatrix} v_{in}(t) \\ i_{in}(t) \end{bmatrix}$$

Problems 5 and 6 refer to the following system



5) To reduce the sensitivity of the closed loop transfer function variations in the plant G_p , we should

a) make $|G_c(j\omega)G_p(j\omega)H(j\omega)|$ large b) make $|G_c(j\omega)G_p(j\omega)H(j\omega)|$ small

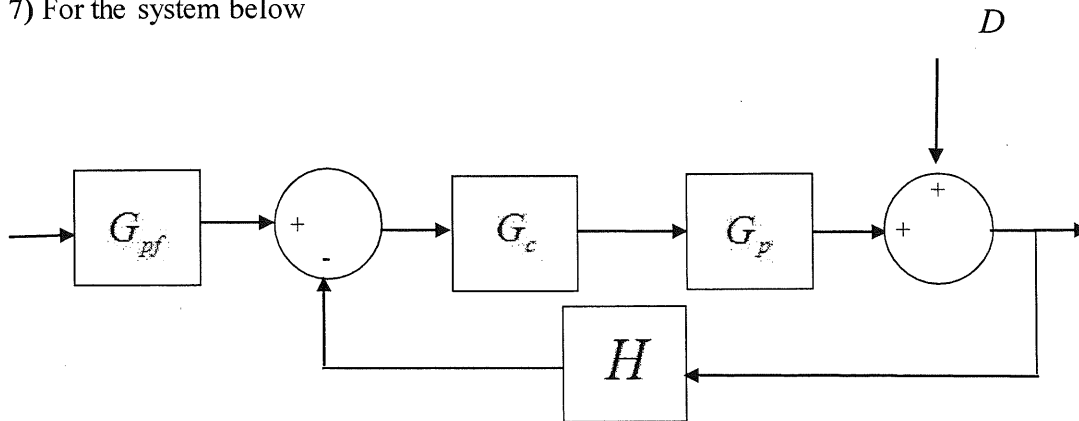
c) make G_{pf} large d) do nothing, we cannot change the sensitivity

6) To reduce the sensitivity of the closed loop transfer function to variations in the sensor H , we should

a) make $|G_c(j\omega)G_p(j\omega)H(j\omega)|$ large b) make $|G_c(j\omega)G_p(j\omega)H(j\omega)|$ small

c) make G_{pf} large d) do nothing, we cannot change the sensitivity

7) For the system below

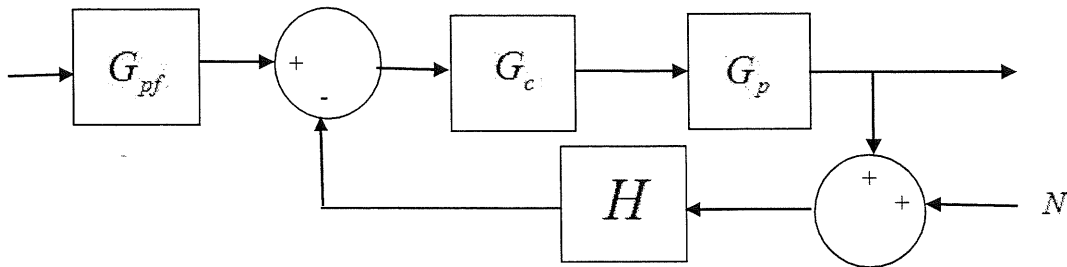


to reduce the effects of the external disturbance D on the system output, we should

a) make $|G_c(j\omega)G_p(j\omega)H(j\omega)|$ large b) make $|G_c(j\omega)G_p(j\omega)H(j\omega)|$ small

c) make G_{pf} large d) do nothing, we cannot change the sensitivity

8) For the system below



to reduce the effects of sensor noise N on the closed loop system , we should

- a) make $|G_c(j\omega)G_p(j\omega)H(j\omega)|$ large b) make $|G_c(j\omega)G_p(j\omega)H(j\omega)|$ small
 c) make $|H(j\omega)|$ large d) do nothing, we cannot change the sensitivity

9) Consider a plant that is unstable but is a controllable system. Is it possible to use state variable feedback to make this system stable?

- a) Yes b) No

10) Is it possible for a system with state variable feedback to change the zeros of the plant (other than by pole-zero cancellation) ?

- a) Yes b) No

11) Is it possible for a system with state variable feedback to introduce zeros into the closed loop system?

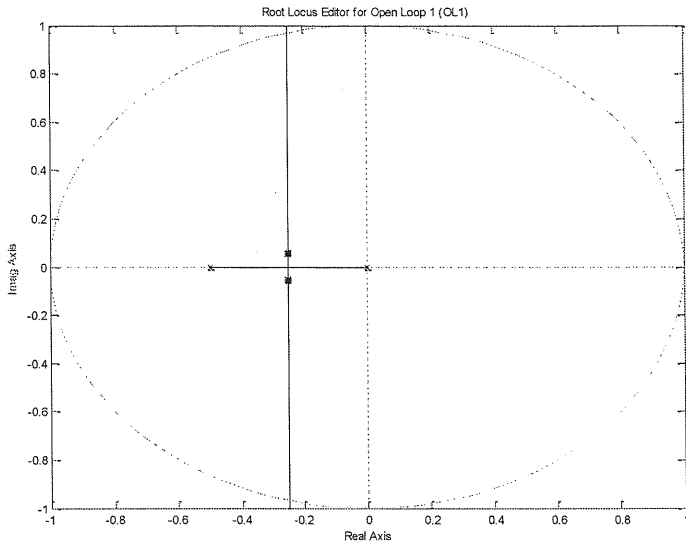
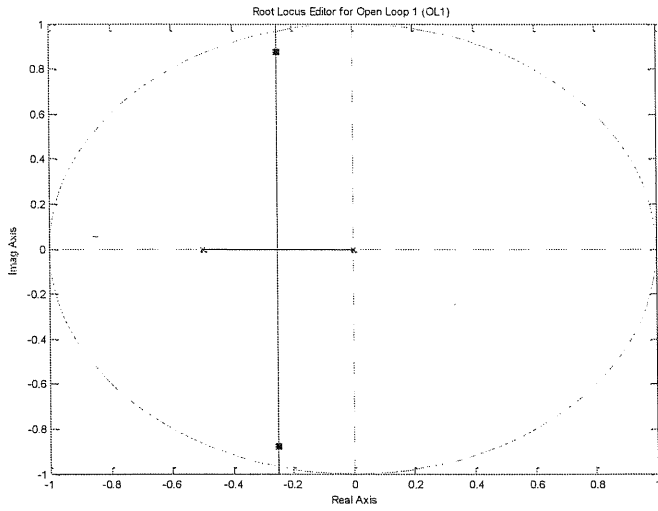
- a) Yes b) No

12) If a plant has n poles, then a system with state variable feedback with no pole-zero cancellations will have

- a) more than n poles b) less than n poles c) n poles d) it is not possible to tell

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Problems 13 and 14 refer to the following two root locus plot for a discrete-time system



13) For which system is the settling time likely to be smallest?

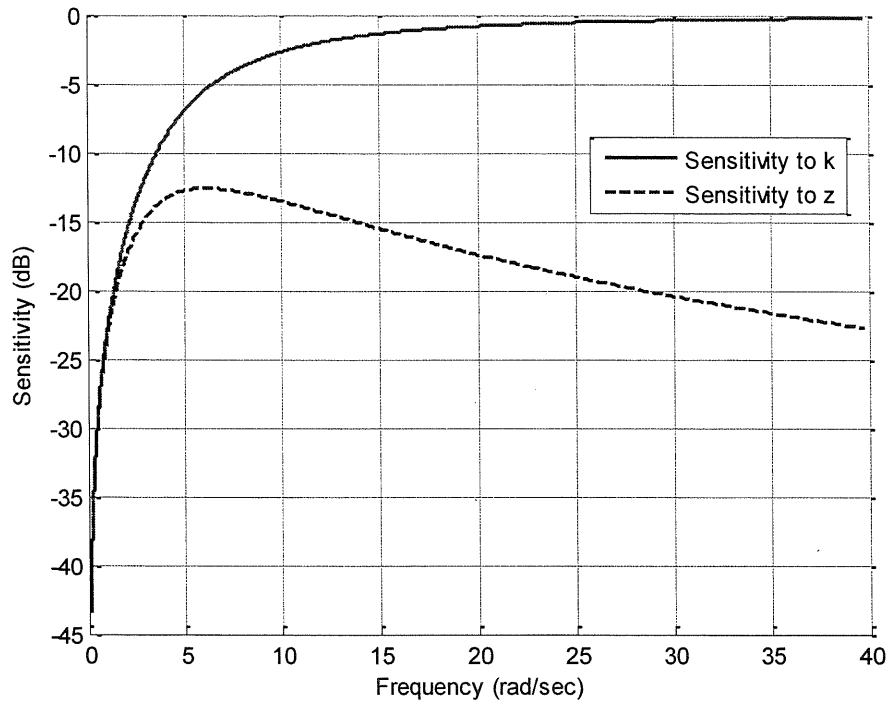
- a) The system on the top b) the system on the bottom c) the settling time will be the same

14) Is this a type 1 system?

- a) yes b) no c) not enough information

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15) The graph below shows a plot of the sensitivities to two parameters. Over this frequency range, the system is more sensitive to which parameter?



more sensitive to k